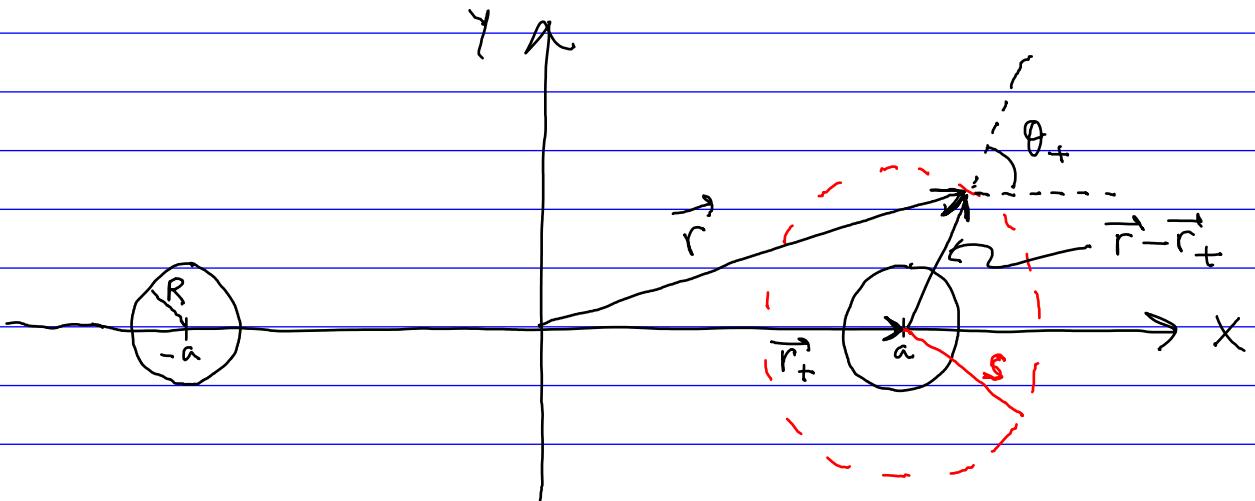


Example : Maxwell stress tensor for two charged cylinders

Two cylinders of radius  $R$  are positioned as shown in the figure below. Both extend indefinitely along the  $z$  axis. We assume that each cylinder has a uniform charge density on the cylinder surface. Let the surface charge density be  $\sigma_+ (\sigma_-)$  on the "+" ("") cylinder centered at  $x = +a$  ( $x = -a$ ).



The electric field  $\vec{E}_\pm$  produced by the  $\pm$ -cylinder can, due to its high symmetry, most easily be found from Gauss's law. Picking the Gaussian surface to be a cylinder of length  $l$  and radius  $s (> R)$  centered at the cylinder, there is no contribution from the two "end faces" (with normal vector  $\hat{n} = \pm \hat{z}$ ) since  $E_{\pm z} = 0$  by symmetry. Symmetry also dictates that  $\vec{E}_\pm$  points radially from each cylinder center and that its magnitude only depends on  $r$ . Gauss's law thus gives (where  $E_\pm$  is the radial component)

$$\oint_S \vec{E}_\pm \cdot d\vec{a} = \frac{Q_{\text{inside}}}{\epsilon_0} \xrightarrow{s \gg R} E_\pm \cdot 2\pi s l = \frac{\sigma_\pm \cdot 2\pi R l}{\epsilon_0}$$

$$\Rightarrow E_{\pm} = \frac{\sigma_{\pm} R}{\epsilon_0 s} = \frac{\sigma_{\pm} R}{\epsilon_0 \sqrt{(x \mp a)^2 + y^2}} \quad (\text{same sign as } \sigma_{\pm})$$

(valid for  $s > R$ )

Let  $\vec{R}_{\pm} \equiv \vec{r} - \vec{r}_{\pm}$ , where  $\vec{r}_{\pm} = (\pm a, 0)$  is the position vector of the  $\pm$  cylinder. Then

$$E_{\pm,x} = E_{\pm} \cos \theta_{\pm}, \quad E_{\pm,y} = E_{\pm} \sin \theta_{\pm}$$

$$\text{where } \cos \theta_{\pm} = \hat{\vec{R}}_{\pm} \cdot \hat{x} = \frac{\vec{r} - \vec{r}_{\pm}}{\|\vec{r} - \vec{r}_{\pm}\|} \cdot \hat{x} = \frac{x \mp a}{\sqrt{(x \mp a)^2 + y^2}}$$

$$\text{and } \sin \theta_{\pm} = \frac{y}{\sqrt{(x \mp a)^2 + y^2}}$$

$$\Rightarrow E_{\pm,x} = \frac{\sigma_{\pm} R}{\epsilon_0} \frac{x \mp a}{(x \mp a)^2 + y^2} \quad \left. \begin{array}{l} \text{valid for regions} \\ \text{outside } \pm \text{ cylinder,} \\ \text{respectively (inside,} \\ E_{\pm} = 0) \end{array} \right\}$$

$$E_{\pm,y} = \frac{\sigma_{\pm} R}{\epsilon_0} \frac{y}{(x \mp a)^2 + y^2}$$

The components of the total electric field  $\vec{E} = \vec{E}_+ + \vec{E}_-$  are then  $E_x = E_{+,x} + E_{-,x}$   
 $E_y = E_{+,y} + E_{-,y}$

The total force on a cylinder can be calculated from

$$\vec{F} = \oint_{\partial S} \vec{T} \cdot d\vec{a}$$

where  $\vec{T}$  is Maxwell's stress tensor for the problem and  $\partial S$  is a surface

enclosing the volume  $\Omega$  which includes the cylinder of interest (and none of the other cylinders). Since  $\vec{E}$  is in the  $xy$  plane only  $F_x$  and  $F_y$  need to be considered. (In fact,  $F_y = 0$  by symmetry, which we will also verify explicitly.) So let us consider

$$F_x = \oint_{\partial\Omega} (T_{xx} dx_x + T_{xy} dx_y + T_{xz} dx_z)$$

$$F_y = \oint_{\partial\Omega} (T_{yx} dx_x + T_{yy} dx_y + T_{yz} dx_z)$$

We have, for this problem,

$$T_{xx} = -T_{yy} = \frac{\epsilon_0}{2} (E_x^2 - E_y^2)$$

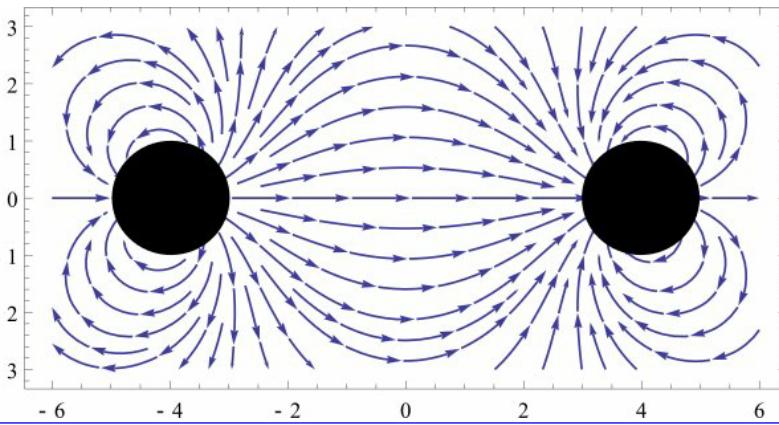
$$T_{xy} = T_{yx} = \epsilon_0 E_x E_y$$

$$T_{yz} = T_{xz} = 0$$

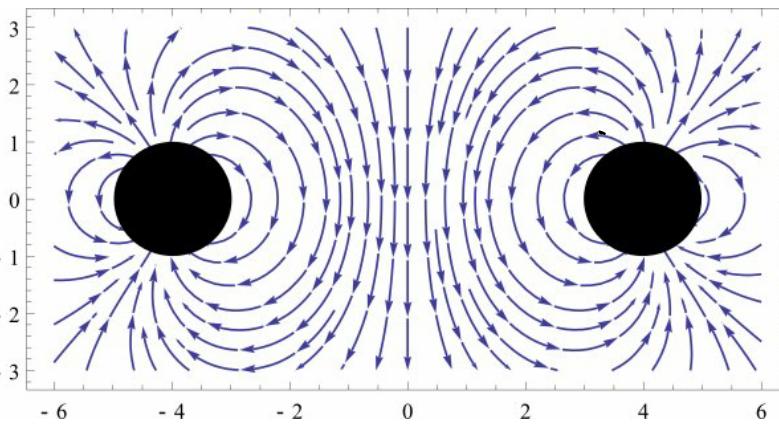
Vector field plots of  $(T_{xx}, T_{xy})$  (relevant for the calculation of  $F_x$ ) and  $(T_{yx}, T_{yy})$  (relevant for the calculation of  $F_y$ ) are shown below for the two cases

$\sigma_- = -\sigma_+$  (cylinders with opposite charges) and  $\sigma_- = \sigma_+$  (— same charges). Note that only the relative sign of the charges matter for  $T$ , not which cylinder has which sign of the charge, since  $\vec{T}$  is invariant under  $\vec{E} \rightarrow -\vec{E}$ .

## Opposite charges

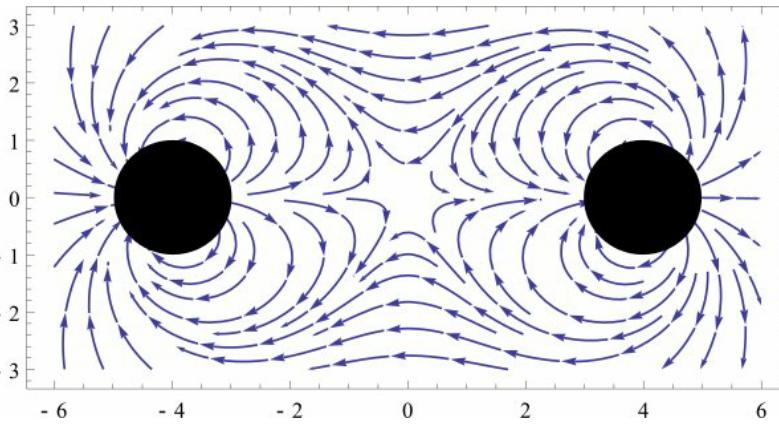


$$(\tau_{xx}, \tau_{xy})$$

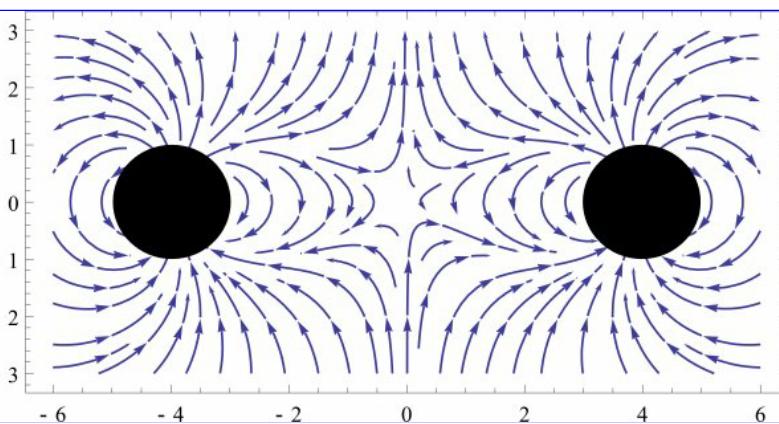


$$(\tau_{yx}, \tau_{yy})$$

## Same charges



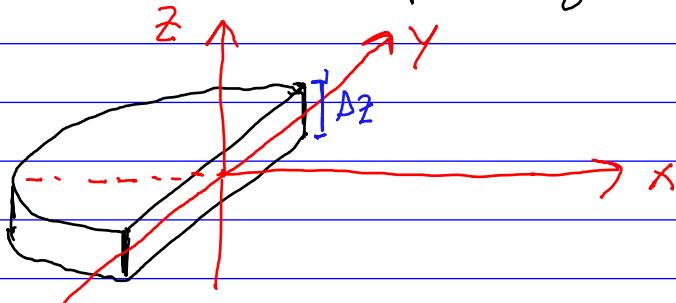
$$(\tau_{xx}, \tau_{xy})$$



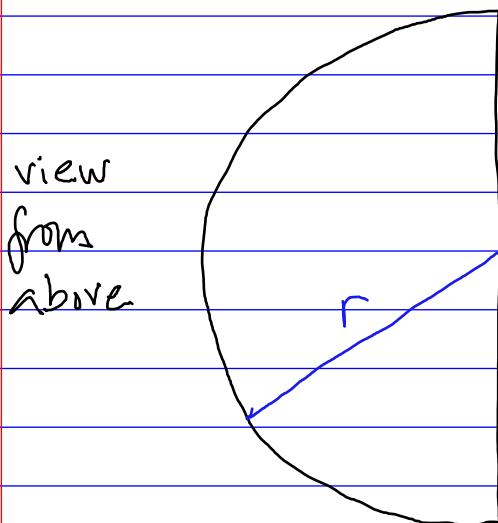
$$(\tau_{yx}, \tau_{yy})$$

For concreteness let us calculate  $F_x$  and  $F_y$  on the left (" - ") cylinder. The volume  $\Omega$  can be any volume enclosing this cylinder and none of the others. For symmetry reasons a good choice is to pick  $\Omega$  to be the region  $x < 0$ , i.e. the left "half-space".

Consider the following finite volume:



The base area is shaped like a semi-circle with radius  $r$ .  
The height is  $\Delta z$



For  $r \gg R, a$ , the electric field on the circular part of the boundary decays with  $r$  as  $1/r$  (or faster, if the two cylinders have  $\sigma_+ = -\sigma_-$ ).  
For the nonzero  $T_{ij}$  coefficients,  $T_{ij} \sim E^2 \sim (1/r)^2 = 1/r^2$ , so the contribution to  $\int \vec{T} \cdot d\vec{a}$  from the circular part of the boundary scales like

$$\left(\frac{1}{r^2}\right) \cdot \frac{2\pi r}{2} \cdot \Delta z \propto \frac{1}{r}, \text{ which } \rightarrow 0 \text{ as } r \rightarrow \infty$$

Also, the contribution from the top and bottom surfaces vanish since  $T_{xz} = T_{yz} = 0$ . Thus in the limit  $r \rightarrow \infty$  the only contribution to  $\int \vec{T} \cdot d\vec{a}$  comes from the boundary at  $x = 0$ . Letting  $\Delta z \rightarrow 0$  this becomes the plane  $x = 0$  ( $yz$  plane).

For  $F_x$  we get

$$F_x = \int_{\substack{x=0 \\ \text{plane}}} (T_{xx}, T_{xy}) \cdot (\underline{d}x, \underline{d}y)$$

$$= (\underline{d}x, 0) \quad \text{since } \hat{n} = \hat{e}_x$$

(  $\hat{n}$  points out of the volume  
x < 0 )

$$= \int_{-\infty}^{\infty} T_{xx}(x=0, y) dy L \quad \text{where } L \text{ is the cylinder length}$$

Since  $L = \infty$ ,  $F_x$  obviously diverges. Let us therefore calculate the force per unit length given by

$$\left( \lim_{L \rightarrow \infty} \right) \frac{F_x}{L} = \int_{-\infty}^{\infty} dy T_{xx}(x=0, y)$$

$$= \frac{\epsilon_0}{2} \int_{-\infty}^{\infty} dy \left[ E_x^2(x=0, y) - E_y^2(x=0, y) \right]$$

$$= \frac{\epsilon_0}{2} \left( \frac{R}{\epsilon_0} \right)^2 \int_{-\infty}^{\infty} dy \frac{1}{(a^2 + y^2)^2} \left\{ (\sigma_+(-a) + \sigma_- a)^2 - (\sigma_+ y + \sigma_- y)^2 \right\}$$

$$= \frac{R^2}{2\epsilon_0} \int_{-\infty}^{\infty} dy \frac{1}{(a^2 + y^2)^2} \left\{ a^2 (\sigma_+ - \sigma_-)^2 - y^2 (\sigma_+ + \sigma_-)^2 \right\}$$

$$= \frac{R^2}{2\epsilon_0} \left\{ \frac{\pi}{2} \frac{1}{a^3} \cdot a^2 (\sigma_+ - \sigma_-)^2 - \frac{\pi}{2a} (\sigma_+ + \sigma_-)^2 \right\}$$

↑ looking up the integrals

$$= \frac{\pi R^2}{4\epsilon_0 a} \left\{ (\sigma_+ - \sigma_-)^2 - (\sigma_+ + \sigma_-)^2 \right\}$$

For opposite charges ( $\sigma_+ = -\sigma_- \equiv \sigma$ ) this gives

$$\underline{\underline{\frac{F_x}{L} = \frac{\pi R \sigma^2}{\epsilon_0 a}}} \quad (>0, \text{ so attracted by right cyl.})$$

while for same charges ( $\sigma_+ = \sigma_- \equiv \sigma$ )

$$\underline{\underline{\frac{F_x}{L} = -\frac{\pi R \sigma^2}{\epsilon_0 a}}} \quad (<0, \text{ so repelled by right cyl.})$$

Thus as expected,  $F_x$  has the same magnitude in both cases but opposite sign. (This result can be shown to be identical to the force/length experienced between two infinite line charges a distance  $2a$  apart, if the charge per unit length is the same as for the cylinders, a reasonable result given that the cylinder charge is assumed from the outset to be uniform.)

Finally,

$$F_y = \int_{x=0}^{\infty} T_{yx} dx = L \epsilon_0 \int_{-\infty}^{\infty} dy E_x(x=0,y) E_y(x=0,y)$$

$$\Rightarrow \underline{\underline{\frac{F_y}{L} = \epsilon_0 \left(\frac{R}{\epsilon_0}\right)^2 \int_{-\infty}^{\infty} dy \frac{a}{(a^2 + y^2)^2} (-\sigma_+ + \sigma_-)(\sigma_+ + \sigma_y) y}} = 0$$

We see that  $F_y = 0$  not only for the two cases of identical and opposite charges, but also more generally due to the integrand being odd in  $y$ .